

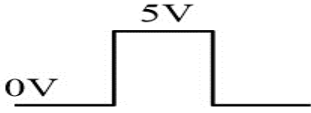
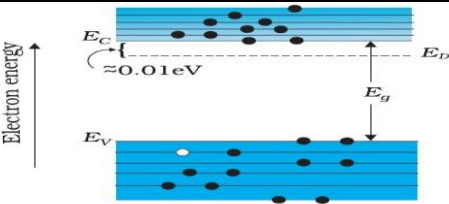
Class: XII Session 2023-24

Additional Practice Question Paper

SUBJECT: PHYSICS(THEORY)

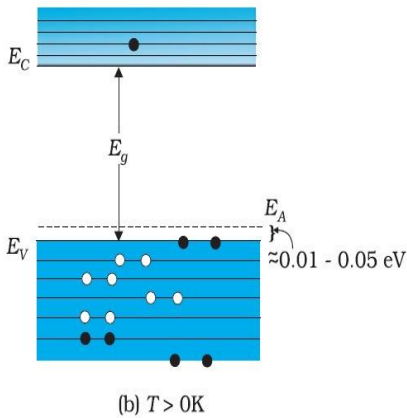
MARKING SCHEME

SN O.	DESCRIPTION	TOTAL MARKS
A1	c	1
A2	b	1
A3	c	1
A4	b	1
A5	c	1
A6	b	1
A7	c	1
A8	d	1
A9	b	1
A10	b	1
A11	b	1
A12	a	1
A13	c	1
A14	a	1
A15	b	1
A16	c	1
SECTION B		
A17	$E = hc/\lambda = 1245/\lambda(\text{nm})$ in eV = $1245/400 = 3.1\text{eV}$ 1 Mo will not emit as work function is more than energy incident 1 OR $p_c = p_A + p_B = h/\lambda_A + h/\lambda_B = h/\lambda_C$ 1 $\lambda_C = \lambda_A \lambda_B / (\lambda_A + \lambda_B)$ 1	2
A18	The position of the n th bright fringe $x = \frac{n\lambda D}{d}$ 1 $\lambda = \frac{xd}{nD} = \frac{(1.2 \times 10^{-2}) \times (0.28 \times 10^{-3})}{4 \times 1.4} = 6000 \text{ \AA}$ 1	2
A19	(a) The direction of motion of the em wave is along negative Y-axis. 1 M (b) Given, $\mathbf{E} = [3.1 \text{ N/C}] \cos [(1.8 \text{ rad/m})y + 5.4 \times 10^8 \text{ rad/s}]t \hat{i}$ Comparing with $E = E_0 \cos [ky + \omega t]$ $K = 1.8 \text{ rad/m}$, $\omega = 5.4 \times 10^8 \text{ rad/s}$ and $E_0 = 3.1 \text{ N/C}$ 1M $\lambda = 2\pi/k = 3.5\text{m}$	2
A20	The electrical potential energy of the two identical nuclei	

	$U = K (50e) (50e) / 2R = \frac{1}{2} \frac{(9 \times 10^9 \times 50 \times 1.6 \times 10^{-16})^2}{2 \times 1.28 \times 10^{-15} \times (125)^{1/3}}$ $= 4.5 \times 10^{-11} \text{ J}$	2
A21	$I = \frac{E+E}{R+r_1+r} \quad V_1 = E - Ir_1 = E - \frac{2E}{r_1+r_2+R} r_1 = 0$ $E = \frac{2Er_1}{r_1+r_2+R}, \quad 1 = \frac{2r_1}{r_1+r_2+R} \quad R = r_1 - r_2$	2
SECTION C		
A22	<p>(a) The electric field intensity is $E = V/d, = \frac{0.50 \text{ V}}{5.0 \times 10^{-7} \text{ m}} = 1.0 \times 10^6 \text{ Vm}^{-1}$.</p>  <p>(b) $0V$</p> <p>(c) Rectifier</p>	3
A23	<p>Applying Kirchhoff's junction rule:</p> $I_1 = I + I_2$ <p>Kirchhoff's loop rule gives:</p> $10 = 2I + 10I_1 = 2I + (10I + I_2)$ $5 = I_2 + 6I \text{-----(1)}$ $2 = 5 I_2 - 2I \text{..... (ii)}$ $I = 5/8A, \quad V = 1.25 \text{ Volt}$	3
A24	<p>(a) The width of central maximum $= 2\lambda D/d$ When the slit width d is doubled, the width of the central maximum is halved. Its area becomes one fourth and hence the intensity becomes four times the initial intensity.</p> <p>(b) When red light is replaced by blue light the linear width of the central maximum decreases because the wavelength of blue light is lesser than that of red light.</p>	3
A25	 <p>(a) $T > 0K$ one thermally generated electron-hole pair + 9 electrons from donor atoms</p>	3

N type and majority charge carriers are electrons.
The number density of electrons to the number density of holes is much greater than 1 for N type semiconductor.

OR



p- type and majority charge carriers are Holes.
The number density of electrons to the number density of holes is much smaller than 1 for N type semiconductor.

A26 **(a) A is Paramagnetic & B is Diamagnetic** **1M**
(b)The magnetic susceptibility of A is positive and that of B is negative. **1M**
(c) The ball will move away from the magnet due to diamagnetic behavior. On being brought near a bar magnet, it will be feebly magnetized opposite to the direction of the magnetizing field and thus it will be repelled. **1M**

3

A27

3

1M

For the first point source O_1

$$\frac{1}{v} - \frac{1}{u} = \frac{1}{f} \quad , \quad \frac{1}{v} - \frac{1}{(-x)} = \frac{1}{9}$$

$\frac{1}{2} M$

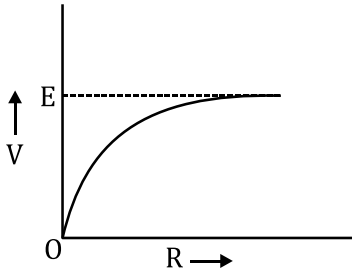
$$\frac{1}{v} = \frac{1}{9} - \frac{1}{x} \quad \dots(i)$$

For the second point source O_2

$$\frac{1}{v} - \frac{1}{(24-x)} = \frac{1}{(-9)}$$

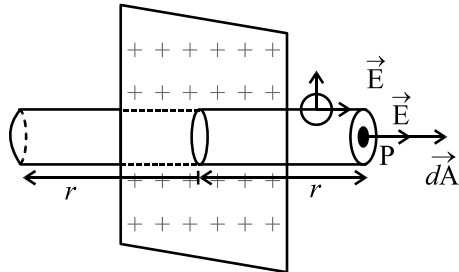
$\frac{1}{2} M$

$$\frac{1}{v} = \frac{-1}{9} + \frac{1}{(24-x)} \quad \dots(ii)$$

	<p>From equation (i) and (ii),</p> $\frac{1}{9} - \frac{1}{x} = \frac{-1}{9} + \frac{1}{24-x}, \quad \frac{1}{(24-x)} + \frac{1}{x} = \frac{2}{9}, \quad x = 18 \text{ cm or } 6 \text{ cm.} \quad 1\text{M}$	
A28	<p>(a)</p>  <p style="text-align: right;">1 M</p> <p>The terminal potential difference, V becomes equal to the emf E when R becomes infinitely large. ½ M</p> <p>(b) $r = \left(\frac{E-V}{V}\right)R$ ½ M</p> <p>Let after connecting another identical wire between terminals, the potential difference be V.</p> $\left(\frac{6-5.6}{6}\right)R = \left(\frac{6-V}{V}\right)\frac{R}{2} \quad V = 5.25 \text{ V} \quad 1\text{M}$	3
SECTION D		
A29	1(b) 2(a) 3 (c) 4(a) OR (b)	4
A30	1(a) 2(a) 3 (c) OR (c) 4(d)	4
SECTION E		
A31	<p>(a) The total electric flux coming out of a closed surface is $1/\epsilon_0$ times the net charge enclosed by it. ½ M</p> <p>(b) Electric field due to an infinite plane sheet of charge. Let us consider an infinite thin plane sheet of positive charge having a uniform surface charge density σ.</p> <p>Let P be the point where electric field E is to be found. Let us imagine a cylindrical gaussian surface of length $2r$ and containing P as shown.</p> <p>The net flux through the cylindrical gaussian surface</p> $\begin{aligned} \phi &= \int_{\text{RCF}} EdA \cos 0^\circ + \int_{\text{LCF}} EdA \cos 0^\circ + \int_{\text{CS}} EdA \cos 90^\circ && 1\text{M} \\ &= E.A + EA + 0, \quad \phi = 2 EA && \frac{1}{2}\text{M} \end{aligned}$	5

The total charge enclosed by the gaussian cylinder = σA

Using Gauss's theorem, $2 EA = \frac{\sigma A}{\epsilon_0}$, $E = \frac{\sigma}{2\epsilon_0}$ **1 M**



½ M

(b) The flux through an area is $EA \cos \theta$. Here the flux through the cone is the same as that through the triangular section of the cone in a vertical plane passing through the vertex. The area of this triangular section is $= \frac{1}{2} [2R \times h]$ and is perpendicular to the direction of electric field.

½ M

The electric flux is $E \times \frac{1}{2} (2R \times h) \cos 0^\circ$ i.e., ERh **1.M**

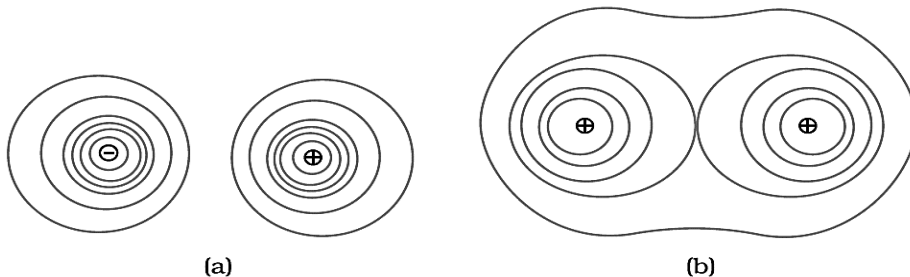
OR

- (a) Equipotential Surfaces
- (b) Three Characteristics
- (c) Numerical

2Marks
1.5Marks
1.5Marks

(a) **EQUIPOTENTIAL SURFACES**

1+1



- (b) 1: Two equipotential surfaces never intersect each other.
2: The electric field intensity is always at right angles to an equipotential surface.
3: The work done in moving a test charge from one point to another point on an equipotential surface is always zero. **3x ½ M**

(c) (i) $E = -\frac{dv}{dx} = \frac{-d}{dx}[5 + 4x^2]$

$E = -8x$. this shows that $E \propto x$, obviously electric field cannot be uniform. 1M .

(ii) At $x = -1\text{m}$, $E = +8 \text{Vm}^{-1}$

\therefore Force on charge of 1C placed at $x = -1 \text{ m}$ is $1 \times 8 = 8 \text{ N}$ $\frac{1}{2} \text{ M}$

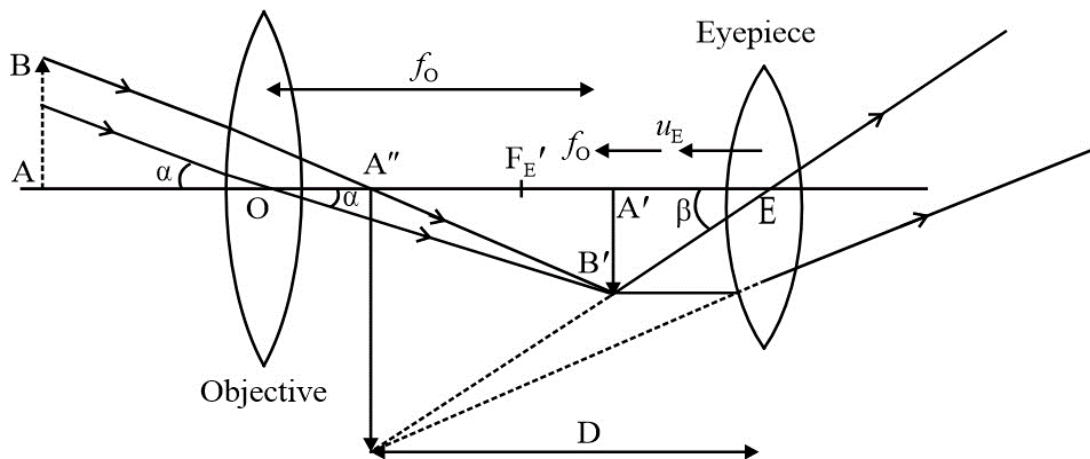
A32

Labelled Ray Diagram:
Magnification:
Numerical:

1.5 M

1.5M

2 M



Magnifying Power:

$$M = \frac{\text{the angle subtended by the final image at the eye when formed at LDDV}}{\text{the angle subtended by the object at the eye when seen directly}}$$

$$= \frac{\beta}{\alpha} = \frac{\tan \beta}{\tan \alpha}$$

...(1)

$$\text{From } \triangle EA'B' \tan \beta = \frac{A'B'}{EA'}$$

...(2)

$$\triangle OA'B' \tan \alpha = \frac{A'B'}{OA'}$$

...(3)

From equations (1), (2) and (3),

$$M = \frac{OA'}{EA'} \Rightarrow M = \frac{+f_o}{-u_e} \quad \dots (4)$$

Case: When the final image is formed at infinity.

$$\frac{1}{v} - \frac{1}{u} = \frac{1}{f} \text{ for eyepiece} \quad \dots (5)$$

Required value of $v = -\infty$, object distance = $-u_e$, focal length = $+f_e$ ---(6)

From (5) & (6), $u_e = f_e$

$$M = \frac{-f_0}{f_E}$$

$$M = -144/6 = -24 \quad \& \quad L = 144 + 6 = 150 \text{ cm.}$$

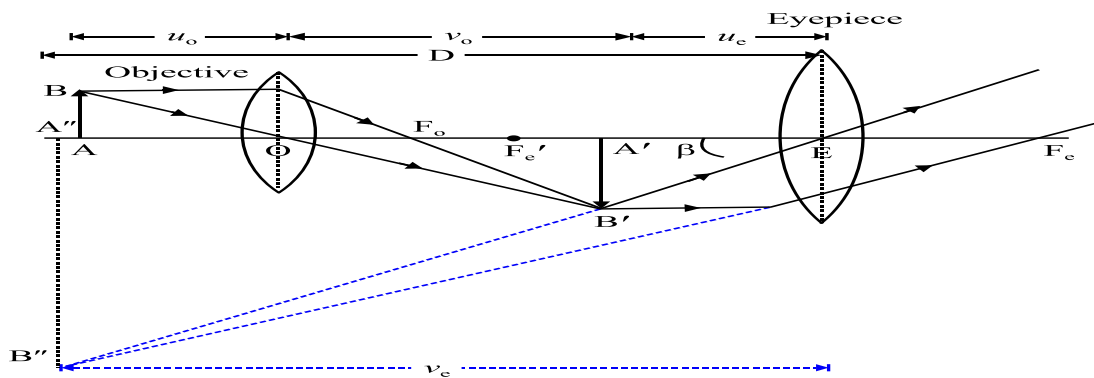
OR

Ray Diagram : 1.5 M

Expression : 1M

Numerical : 2.5M

COMPOUND MICROSCOPE



The magnifying power of compound microscope for final image formed at near point is

$$M = \frac{-v_0}{u_0} \left[+ \frac{D}{f_E} \right]$$

Given, focal length of objective $f_o = 1.25$ cm

Focal length of eyepiece $f_E = 5$ cm

For objective

$$\frac{1}{v_0} - \frac{1}{(-2.5)} = \frac{1}{1.25} \Rightarrow v_0 = 2.5 \text{ cm}$$

$$\text{For eyepiece } \frac{1}{(-\infty)} - \frac{1}{(-u_e)} = \frac{1}{5}$$

$u_e = 5$ cm. So, if the final image is formed at infinity, then the distance between the objective and the eyepiece is $(v_0 + u_e)$ i.e. 7.5 cm.

(a) Expression for Average Power**3M****(b) Reason****1M****(c) Numerical****1M**

(a) Average power in an a.c. circuit

Let the instantaneous values of alternating emf and current applied to an ac circuit be given by

$$e = e_0 \sin \omega t$$

and $i = i_0 \sin (\omega t + \phi)$ where ϕ is the phase difference between A small work done by the ac source in the circuit in the dt is given by

$$dW = e i dt = e_0 i_0 \sin \omega t \sin (\omega t + \phi) dt$$

The total work done by AC source in one complete cycle is

$$\begin{aligned} \int dW &= \int_0^T e i dt = e_0 i_0 \int_0^T \sin \omega t \sin (\omega t + \phi) dt \\ &= e_0 i_0 \int_0^T \sin \omega t [\sin \omega t \cos \phi + \cos \omega t \sin \phi] dt \\ &= e_0 i_0 \int_0^T \cos \phi \sin^2 \omega t dt + e_0 i_0 \int_0^T \sin \phi \sin \omega t \cos \omega t dt \\ &= \frac{e_0 i_0 \cos \phi}{2} \int_0^T (1 - \cos 2\omega t) dt + \frac{e_0 i_0 \sin \phi}{2} \int_0^T \sin 2\omega t dt \end{aligned}$$

$$W = \frac{e_0 i_0 \cos \phi T}{2}$$

\therefore The average power dissipated per cycle is

$$P_{av} = \frac{W}{T} = \frac{e_0}{\sqrt{2}} \frac{i_0}{\sqrt{2}} \cos \phi$$

$$\Rightarrow P_{av} = E_{RMS} \cdot I_{RMS} \cos \phi$$

\therefore True power = Apparent power \times Power factor

(b) To transport a given power, low power factor means large current through the transmission line, resulting in large power loss.

(c) **Case-1** : Given, $X_L = R$

$$\text{Power factor, } P_1 = \frac{R}{\sqrt{R^2 + X_L^2}} = \frac{1}{\sqrt{2}}$$

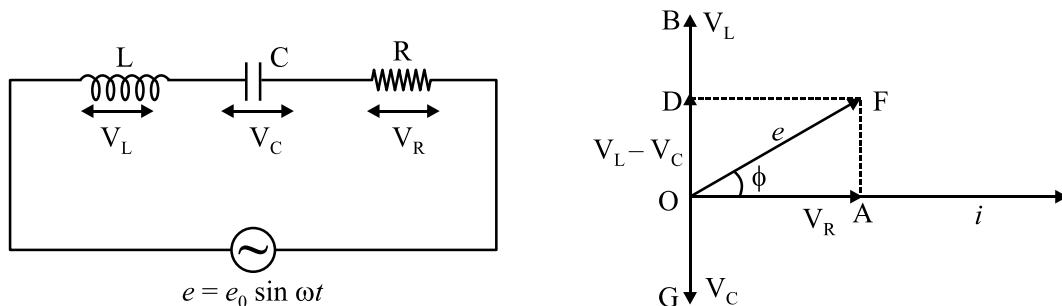
Case-2: Given, $X_L = X_C$

$$Z = \sqrt{R^2 + (X_L - X_C)^2} = R$$

$$\text{Power factor} = \frac{R}{Z} = \frac{R}{R} = 1 \quad \therefore \frac{P_1}{P_2} = \frac{1}{\sqrt{2}}$$

- OR**
- (a) Phasor Diagram : 1/2 M**
Expression for Current : 1M
Phase angle : 1M
Condition for Resonance : 1M
(b) Proof : 1.5M

An ac circuit containing an inductor, a capacitor and a resistor in series.



Let an alternating emf $e = e_0 \sin \omega t$ be applied to LCR series combination.

Let i be the current in the circuit at any instant of time and V_R , V_L and V_C be the voltages across R, L and C respectively at that instant. Then

$$V_R = iR, V_L = iX_L \text{ and } V_C = iX_C$$

Now V_R is in phase with i , V_L leads i by 90° while V_C lags behind i by 90° . In the phasor diagram, the vector OA is representing V_R which is in phase with i , the vector OB represent V_L (which leads i by 90°) and the vector OG is representing V_C (which lags behind i by 90°). If $V_L > V_C$ then their resultant will be $(V_L - V_C)$ which is represented by the vector OD . The vector OF is representing the resultant of V_R and $(V_L - V_C)$. Thus,

$$e = \sqrt{V_R^2 + [V_L - V_C]^2}$$

$$e = i \sqrt{R^2 + (X_L - X_C)^2}$$

$$i = \frac{e}{\sqrt{R^2 + (X_L - X_C)^2}}$$

Here, $\sqrt{R^2 + (X_L - X_C)^2}$ is the effective resistance or impedance of the circuit.

Therefore,

$$Z = \sqrt{R^2 + (X_L - X_C)^2}$$

$$\text{As } X_L = \omega L \text{ and } X_C = 1/\omega C$$

$$\therefore Z = \sqrt{R^2 + \left(\omega L - \frac{1}{\omega C}\right)^2}$$

The phasor diagram shows that in LCR series circuit, the applied emf e leads the current i by a phase angle ϕ , given by

$$\tan \phi = \frac{V_L - V_C}{V_R} = \frac{X_L - X_C}{R} = \frac{\omega L - 1/\omega C}{R}$$

The following 3 cases arise:

- (i) If $X_L > X_C$, then ϕ is positive. In this case the emf e leads the current i
- (ii) If $X_L < X_C$, then ϕ is negative. In this case the emf e lags behind the current
- (iii) If $X_L = X_C$, then $\phi = 0$. In this case the emf e and the current i are in phase and $Z = R = \text{minimum}$. This is the case of series resonance. Hence at resonance

$$X_L = X_C$$

$$\omega L = 1/\omega C \quad \Rightarrow \quad \boxed{\omega = 1/\sqrt{LC}}$$

$$2\pi f L = \frac{1}{2\pi f C} \quad \Rightarrow \quad \boxed{f = \frac{1}{2\pi\sqrt{LC}}} \text{ Resonant linear frequency.}$$

(b)

Given: $Z_{f_1} = Z_{f_2}$

As R is same in both cases

$$X_{f_1} = X_{f_2}$$

$$(X_L - X_C)_{f_1} = (X_C - X_L)_{f_2}$$

$$(X_L)_{f_1} + (X_L)_{f_2} = (X_C)_{f_2} + (X_C)_{f_1}$$

$$2\pi L(f_1 + f_2) = \frac{1}{2\pi C} \left(\frac{1}{f_1} + \frac{1}{f_2} \right)$$

$$2\pi L(f_1 + f_2) = \frac{1}{2\pi C} \frac{(f_1 + f_2)}{f_1 f_2}$$

$$4\pi^2 LC = \frac{1}{f_1 f_2}$$

$$2\pi\sqrt{LC} = \frac{1}{\sqrt{f_1 f_2}}$$

$$\text{Resonant frequency} = \frac{1}{2\pi\sqrt{LC}} = \sqrt{f_1 f_2}$$

